

SIL Calculations

Practical Guidance in the used of IEC 61508-6:2010

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Our Members





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Who Are We?

- We are a cross-industry group of organisations with a common interest in functional safety, particularly in applying IEC 61508 and related standards (e.g., IEC 61511, IEC 62061) correctly in order to demonstrate compliance and improve safety for all.
- Our members include end-users (from many industry sectors), EPC companies, systems integrators, product manufacturers, consultants and certifiers. We also have active relationships with related industry organisations and safety regulators who often attend our meetings.
- We develop and publish many useful and informative guides and assessment tools which are available to all (not just our members) and are free of charge.



In This Workshop:

- We will look at the simplified formulas for the Reliability Block Diagram methodology given in IEC 61508:2010, Part 6, Annex B.
- We will then use the method to calculate the average Probability of Failure on Demand for a typical low demand example SIF from the process industry.
- We will consider the effects that imperfect testing and common cause factors have on the results of the calculations.





You have an understanding of why we quantify random hardware failures in Functional Safety.

• You understand the difference between modes of operation.

 For the purpose of this workshop we will focus on Demand Mode SIFs since this is the most common mode of operation in the Process Industry sector



Mode of Operation

In Demand Mode the target failure measure is in the following format:

- Uses average Probability of Failure on Demand (PFDavg)
- Takes credit for proof testing
- Takes credit for diagnostics

| | Demand Mode of Operation | | | | | | |
|-----|--|-----------------------|--|--|--|--|--|
| SIL | Average probability of failure on demand | Target risk reduction | | | | | |
| 4 | ≥10 ⁻⁵ to <10 ⁻⁴ | >10,000 to ≤100,000 | | | | | |
| 3 | ≥10 ⁻⁴ to <10 ⁻³ | >1,000 to ≤10,000 | | | | | |
| 2 | ≥10 ⁻³ to <10 ⁻² | >100 to ≤1,000 | | | | | |
| 1 | ≥10 ⁻² to <10 ⁻¹ | >10 to ≤100 | | | | | |



Quantifying Random Hardware Failures

IEC 61508-6:2010 Annex B:

Examples of Technique for Evaluating Probabilities of Hardware Failure

Simplified Reliability Block Diagram

Fault Tree

State / Transitions approach (Markov / Petri net)

The methodology will depend on complexity

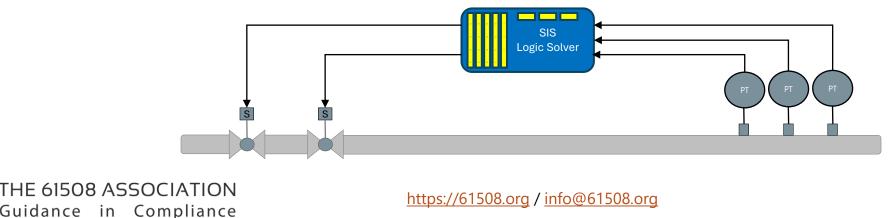
More often than not, we can use the Reliability Block Diagram approach using simplified formulas to approximate PFD_{avg}

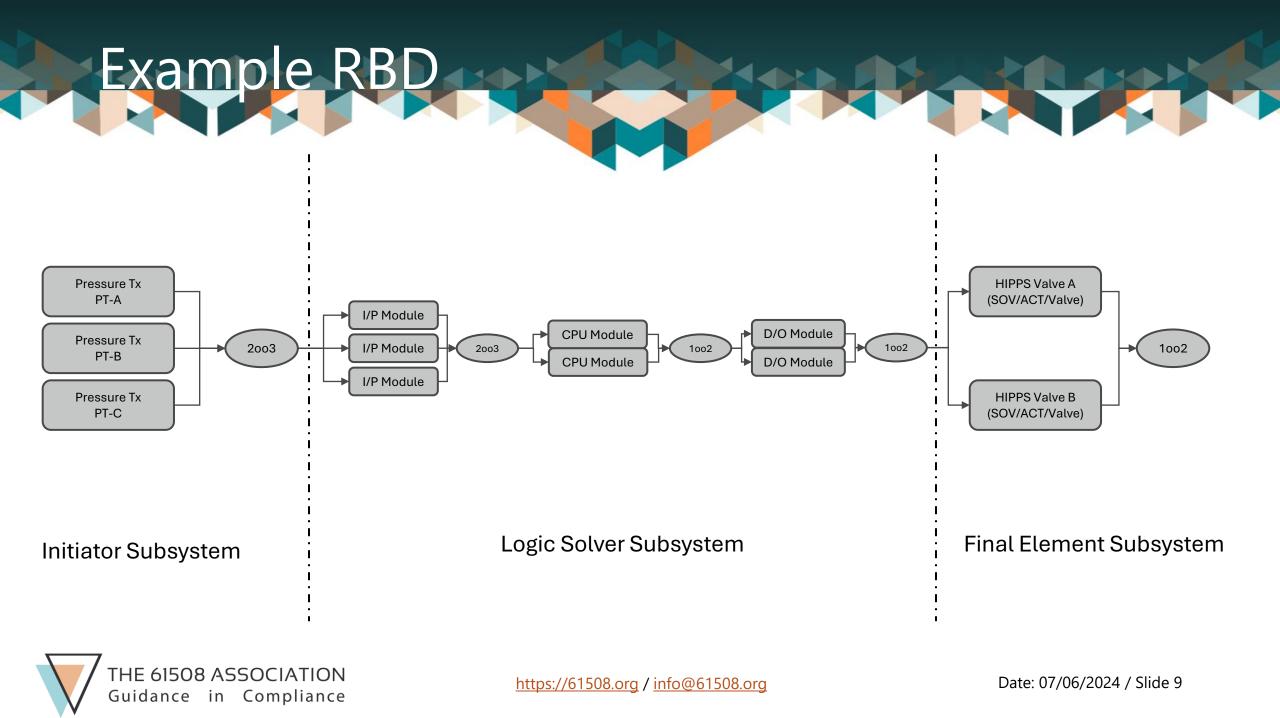


Example Using RBD

Using an example SIF we will go through the RBD methodology from IEC 61508-6 Annex B to calculate the average Probability of Failure on Demand.

- 1. Split the SIF into three subsystems (Initiators, Logic Solver, Final Elements)
- 2. Produce a simplified RBD for each subsystem complete with voting architectures
- 3. Apply the simplified formulas from IEC 61508-6:2010 Annex B to calculate the PFDavg of each subsystem
- 4. Add each subsystem PFDavg together to arrive at the total SIF PFDavg





Simplified Formulas

The following formula are from IEC 61508-6:2010 Annex B.3.2.

For each channel of a subsystem we need to calculate the 'channel equivalent mean down time' (t_{CE})

$$t_{CE} = \frac{\lambda_{DU}}{\lambda_{D}} \left(\frac{T_{1}}{2} + MRT \right) + \frac{\lambda_{DD}}{\lambda_{D}} MTTR$$

For a subsystem made up of redundant channels, we need to calculate the 'system equivalent mean down time' (t_{GE})

$$t_{GE} = \frac{\lambda_{DU}}{\lambda_{D}} \left(\frac{T_{1}}{3} + MRT \right) + \frac{\lambda_{DD}}{\lambda_{D}} MTTR$$

Also a few other channel downtime formulas to consider for other architectures



Simplified Formulas

We then apply the channel downtime to the formula below to determine the subsystem $\mathsf{PFD}_{\mathsf{avg}}$

| Subsystem Architecture | IEC 61508-6:2010 Formula |
|---------------------------|--|
| 1001 | $PFD = (\lambda_{DU} + \lambda_{DD})t_{CE}$ |
| 2002 | $PFD = 2(\lambda_{DU} + \lambda_{DD})t_{CE}$ |
| 1002 | $PFD = 2\left((1-\beta_D)\lambda_{DU} + (1-\beta)\lambda_{DU}\right)^2 tCE tGE + \beta_D \lambda_{DD} MTTR + \beta \lambda_{DU}\left(\frac{T_1}{2} + MRT\right)$ |
| 2003 | $PFD = 6\left((1-\beta_D)\lambda_{DU} + (1-\beta)\lambda_{DU}\right)^2 tCE tGE + \beta_D \lambda_{DD} MTTR + \beta \lambda_{DU}\left(\frac{T_1}{2} + MRT\right)$ |

| PFD | Probability of Failure on Demand |
|-----------------------|---|
| λDU | Dangerous Undetected failure rate |
| λ_{DD} | Dangerous Detected failure rate |
| t _{CE} | Channel equivalent mean down time |
| t _{GE} | System equivalent mean down time |
| β | Common Cause Failure fraction |
| β_D | Common Cause Failure fraction for detected failures |
| MTTR | Mean Time To Restoration |
| MRT | Mean Repair Time |
| T ₁ | Proof Test Interval |



PFD Calculation

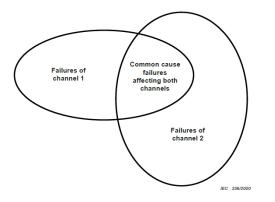
| PFD _{avg} Calculation Results | | | | | | | | |
|--|---|--------------|--------------------------------|--------------------|------------------|--|--|--|
| | | Param | neters | | Architecture | | | |
| Element | I MITR I ' | | β _D factor (CCF) | PFD _{Avg} | | | | |
| Initiator Subsystem | | | | | | | | |
| Pressure Transmitter | 1 year | 8 hours | 10% | 10% | 2003 2.36E-04 | | | |
| | Initia | ator Subsys | tem PFD _{avg} | Subtotal: | 2.36E-04 | | | |
| | | Logic Solver | Subsystem | | | | | |
| A I/P | 1 year | 8 hours | 2% | 1% | 2003 6.97E-07 | | | |
| CPU | 1 year 8 hours 2% | | 2% | 1% | 1002 5.34E-07 | | | |
| D O/P 1 year | | 8 hours | 2% | 1% | 1002 6.68E-07 | | | |
| | Logic So | lver Subsys | tem PFD _{avg} | Subtotal: | 1.90E-06 | | | |
| | F | inal Element | t Subsystem | | | | | |
| Valve Assembly | Valve Assembly 1 year 120 hours 10% 10% | | | | | | | |
| | 1.05E-03 | | | | | | | |
| | 1.29E-03 | | | | | | | |
| | 777 | | | | | | | |

| Safety Instrumented Function Element Failure Rate Data | | | | | | | |
|--|---|--------------------------|----------------|----------------|-----------------|--|--|
| Initiators | Model | Data Source | λ _s | λ_{DD} | λ _{DU} | | |
| Pressure Transmitter | Pressure Transmitter Pressure Transmitter | | 5.00E-07 | 8.00E-07 | 5.00E-07 | | |
| Logic Solver | Model | Data Source | λ _s | λ_{DD} | λ _{DU} | | |
| Analogue Input Module A I/P | | Certificate | 1.13E-06 | 8.86E-07 | 7.06E-09 | | |
| Central Processing Unit | CPU | Certificate | 1.31E-06 | 1.28E-06 | 4.90E-09 | | |
| Digital Output Module | D O/P | Certificate | 9.35E-07 | 8.61E-07 | 6.81E-09 | | |
| Final Elements | Model | Data Source | λ_{s} | λ_{DD} | λ _{ου} | | |
| Solenoid Valve | Solenoid Valve | SINTEF PDS Item 4.3.5 | 1.90E-06 | 1.00E-07 | 6.00E-07 | | |
| HIPPS Valve (incl. Actuator) HIPPS Valve | | SINTEF PDS Item 4.3.3 | 2.00E-06 | 3.00E-07 | 1.50E-06 | | |
| Valve Assembly (sum of above) | Valve Assembly | SINTEF PDS | 3.90E-06 | 4.00E-07 | 2.10E-06 | | |

| Demand Mode of Operation | | | | | |
|---|--|-----------------------|------------------|--|--|
| SIL Average probability of failure on demand | | Target risk reduction | | | |
| 4 | ≥10 ⁻⁵ to <10 ⁻⁴ | >10,000 to ≤100,000 | | | |
| 3 | >10 ⁻⁴ to <10 ⁻³ | >1,000 to ≤10,000 | | | |
| 2 | ≥10 ⁻³ to <10 ⁻² | >100 to ≤1,000 | \triangleright | | |
| 1 | ≥10 ⁻² to <10 ^{-⊥} | >10 to ≤100 |] | | |



Beta Factor Considerations



| Table | D.4 – | Calculation | of β_{int} | or $\beta_{\rm D int}$ |
|-------|-------|-------------|------------------|------------------------|
|-------|-------|-------------|------------------|------------------------|

| Score (S or S _D) | Corresponding value of $m{eta}_{	ext{int}}$ or $m{eta}_{	ext{D int}}$ for the: | | | | |
|------------------------------|--|------------------------------|--|--|--|
| | Logic subsystem | Sensors or final elements | | | |
| 120 or above | 0,5 % | 1 % | | | |
| 70 to 120 | 1 % | 2 % | | | |
| 45 to 70 | 2 % | 5% | | | |
| Less than 45 | 5 % | 10 % | | | |

NOTE 1 The maximum levels of $\beta_{\rm D \ int}$ shown in this table are lower than would normally be used, reflecting the use of the techniques specified elsewhere in this standard for the reduction in the probability of systematic failures as a whole, and of common cause failures as a result of this.

NOTE 2 Values of $\beta_{\rm D\ int}$ lower than 0,5 % for the logic subsystem and 1 % for the sensors would be difficult to justify.

Typically we see the most conservative β values used without proper evaluation

However, from IEC 61508-6:2010 Annex D:

The β_{int} derived from Table D.4 is the common cause failure associated with a 1002 system. For other levels of redundancy (MooN) this β_{int} value will change as given in Table D.5 to yield the final value of β .



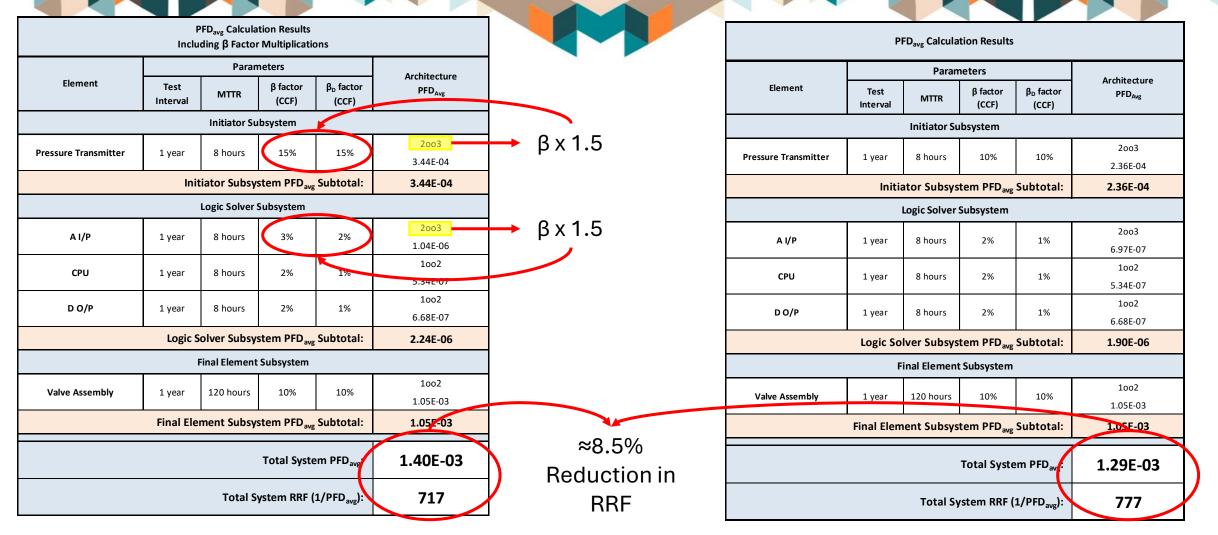
Beta Factor Considerations

Beta Factor for systems with levels of redundancy greater than 1002 should be changed with multiplication factors given in IEC 61508-6:2010 Annex D, Table D.5

| ΜοοΝ | | Ν | | | | | |
|------|---|---------------|-----------------------|------------------------|-----------------------|--|--|
| | | 2 | 3 | 4 | 5 | | |
| М | 1 | β_{int} | 0,5 $\beta_{\rm int}$ | 0,3 β_{int} | 0,2 $\beta_{\rm int}$ | | |
| | 2 | - | 1,5 $eta_{	ext{int}}$ | 0,6 $\beta_{\rm int}$ | 0,4 $\beta_{\rm int}$ | | |
| | 3 | - | - | 1,75 $\beta_{\rm int}$ | 0,8 $eta_{\rm int}$ | | |
| | 4 | - | - | - | $2 \beta_{int}$ | | |



Beta Factor Considerations





Other Considerations

IEC 61508-6:2010, Annex B.3 - Reliability block diagram approach is based on some assumptions listed in Clause B.3.1. These include:

B.3.1 Underlying hypothesis

The calculations are based on the following assumptions:

- the channels in a voted group all have the same failure rates and diagnostic coverage;
- for each safety function, there is perfect proof testing and repair (i.e. all failures that remain undetected are detected by the proof test),

IEC 61511-1:2016, Clause 11.9.2 also states:

11.9.2 The calculated failure measure of each SIF due to random failures shall take into account all contributing factors including the following:

 h) the coverage of any periodic proof tests, the associated proof test procedure and the reliability for the proof test facilities and procedure;



Simplified Formulas with PTC

Fortunately, IEC 61508-6:2010 Annex B.3.2.5 includes formulas considering 'non-perfect proof tests'.

These introduce the concept of Proof Test Coverage (PTC).

- PTC is a measure of how effective the proof test is at revealing Undetected Dangerous Failures.
- Undetected Dangerous Failures that can not be revealed by proof testing remain until the equipment is returned to its 'As New' condition.
- A second test interval (T₂) is introduced as the time interval when the equipment is returned to 'As New'.



Simplified Formulas with PTC

The 'channel equivalent mean down time' (t_{CE}) considering PTC is now:

$$t_{CE} = \frac{\lambda_{DU}(PTC)}{\lambda_{D}} \left(\frac{T_{1}}{2} + MRT\right) + \frac{\lambda_{DU}(1 - PTC)}{\lambda_{D}} \left(\frac{T_{2}}{2} + MRT\right) \frac{\lambda_{DD}}{\lambda_{D}} MTTR$$

The 'system equivalent mean down time' (t_{GE}) considering PTC is now:

$$t_{GE} = \frac{\lambda_{DU}(PTC)}{\lambda_{D}} \left(\frac{T_{1}}{3} + MRT\right) + \frac{\lambda_{DU}(1 - PTC)}{\lambda_{D}} \left(\frac{T_{2}}{3} + MRT\right) \frac{\lambda_{DD}}{\lambda_{D}} MTTR$$



Simplified Formulas with PTC

With the simplified PFDavg formulas now:

| Subsystem Architecture | IEC 61508-6:2010 Formula |
|---------------------------|---|
| 1001 | $PFD = (\lambda_{DU} + \lambda_{DD})t_{CE}$ |
| 2002 | $PFD = 2(\lambda_{DU} + \lambda_{DD})t_{CE}$ |
| 1002 | $PFD = 2\left((1-\beta_D)\lambda_{DU} + (1-\beta)\lambda_{DU}\right)^2 \cdot tCE \cdot tGE + \beta_D \cdot \lambda_{DD} \cdot MTTR + \beta \cdot \lambda_{DU}(PTC)\left(\frac{T_1}{2} + MRT\right) + \beta \cdot \lambda_{DU}(1-PTC)\left(\frac{T_2}{2} + MRT\right)$ |
| 2003 | $PFD = 6\left((1-\beta_D)\lambda_{DU} + (1-\beta)\lambda_{DU}\right)^2 \cdot tCE \cdot tGE + \beta_D \cdot \lambda_{DD} \cdot MTTR + \beta \cdot \lambda_{DU}(PTC)\left(\frac{T_1}{2} + MRT\right) + \beta \cdot \lambda_{DU}(1-PTC)\left(\frac{T_2}{2} + MRT\right)$ |



What PTC to Use?

This depends on the Proof Tests being performed.

For modern, SIL certified initiators (e.g. electronic transmitters) the Safety Manual usually details proof test procedures and the PTC that can be claimed. Usually a good start point but you must consider this is the context of the specific application.

Logic Solver – Usually left at 100% due to the difficulty in testing for the very small dangerous undetected failures. I consider 98% to allow for testing inconsistencies or human errors.



What PTC to Use?

SIF Final Elements (typically valves) do not usually have detailed proof test procedures with corresponding PTC due to the varying applications they are used in.

FMEDA + designed proof test procedures

Compare the proof test procedures against failure modes of an equivalent valve from a generic data source such as OREDA.

| OREDA Based Valve Test Coverage Analysis - ESDV (Taxonomy 4.4.5.1) | | | | | | |
|--|--------------|---------------------------------|--------------------|--|--|--|
| Failure Mode | Failure % | Proof Test Method | Complete in PT? | | | |
| Delayed operation | 11 | Timed operation | Y | | | |
| Failure to close | 32 | Stroke test | Y | | | |
| Internal Leakage | 15 | Leak test | N | | | |
| Structural Deficiency | 24 | Visual inspection + Stroke Test | Y | | | |
| other | 18 | Assumed visual inspection | Y | | | |
| Proof Test Coverage | 85 % | | | | | |



Effect on Overall PFDavg

| PFD _{avg} Calculation Results | | | | | | |
|--|---|------------|-------------------|--------------------------------|-----------|--------------------|
| Considering PTC and β MooN multiplications | | | | | | |
| F laws and | | 1 | Parameters | I | | Architecture |
| Element | Test Interval | MTTR | β factor (CCF) | β _D factor (CCF) | РТС | PFD _{Avg} |
| | | Initia | ator Subsyste | em | | |
| Pressure Transmitter | 1 year | 8 hours | 10% | 10% | 90% | 2003 |
| | т уеаг | 8 110013 | 1078 | 1078 | 5078 | 6.76E-04 |
| | | Init | iator Subsy | stem PFD _{avg} | Subtotal: | 6.76E-04 |
| | | Logic S | Solver Subsys | stem | | |
| A I/P | 1 yoar | 8 hours | 2% | 1% | 98% | 2003 |
| AIJP | 1 year | 8 110015 | 270 | 170 | 98% | 1.21E-06 |
| CPU | 1 year | 8 hours | 2% | 1% | 98% | 1002 |
| 5.0 | i year | onours | 270 | 1/0 | 5070 | 6.12E-07 |
| D O/P | 1 year | 8 hours | 2% | 1% | 98% | 1002 |
| | · | | | | | 7.76E-07 |
| | | Logic S | olver Subsy | stem PFD _{ave} | Subtotal: | 2.60E-06 |
| | | Final El | ement Subsy | stem | | |
| Valve Assembly | 1 year | 120 hours | 10% | 10% | 85% | 1002 |
| valve Assembly | туса | 120 110013 | 1076 | 1076 | 0570 | 2.71E-03 |
| Final Element Subsystem PFD _{avg} Subtotal: | | | | | | 2.71E-03 |
| Total System PFD _{ave} 3.39E-03 | | | | | | 3.39E-03 |
| | Total System RRF (1/PFD _{avg}): 295 | | | | | |

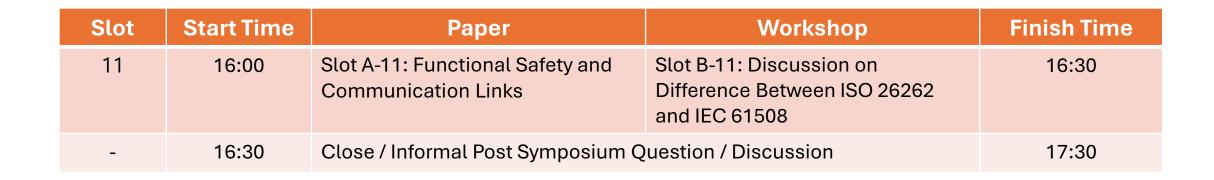
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| | | PFD _{avg} Calcula ding β Factor | | ons | |
|--|------------------|---|-------------------|--------------------------------|------------------------------------|
| Element | Parameters | | | | Architosturo |
| | Test Interval | MTTR | β factor (CCF) | β _D factor (CCF) | Architecture PFD _{Avg} |
| | | Initiator Su | bsystem | | |
| Pressure Transmitter | 1 year | 8 hours | 15% | 15% | 2003 3.44E-04 |
| Initiator Subsystem PFD _{avg} Subtotal: | | | | | 3.44E-04 |
| Logic Solver Subsystem | | | | | |
| A I/P | 1 year | 8 hours | 3% | 2% | 2003 1.04E-06 |
| CPU | 1 year | 8 hours | 2% | 1% | 1002 5.34E-07 |
| D O/P | 1 year | 8 hours | 2% | 1% | 1002 6.68E-07 |
| Logic Solver Subsystem PFD _{avg} Subtotal: | | | | | 2.24E-06 |
| Final Element Subsystem | | | | | |
| Valve Assembly | 1 year | 120 hours | 10% | 10% | 1002 1.05E-03 |
| Final Element Subsystem PFD _{avg} Subtotal: | | | | | 1.05E-03 |
| Total System PFD _{avg} | | | | | 1.40E-03 |
| Total System RRF (1/PFD _{avg}): | | | | | 717 |



Presenter:Ian Dolan – Principal ConsultantContact Details:idolan@sellacontrols.comWhat's next....



We would be more than happy to discuss membership with you (<u>https://61508.org/membership/</u>)

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